

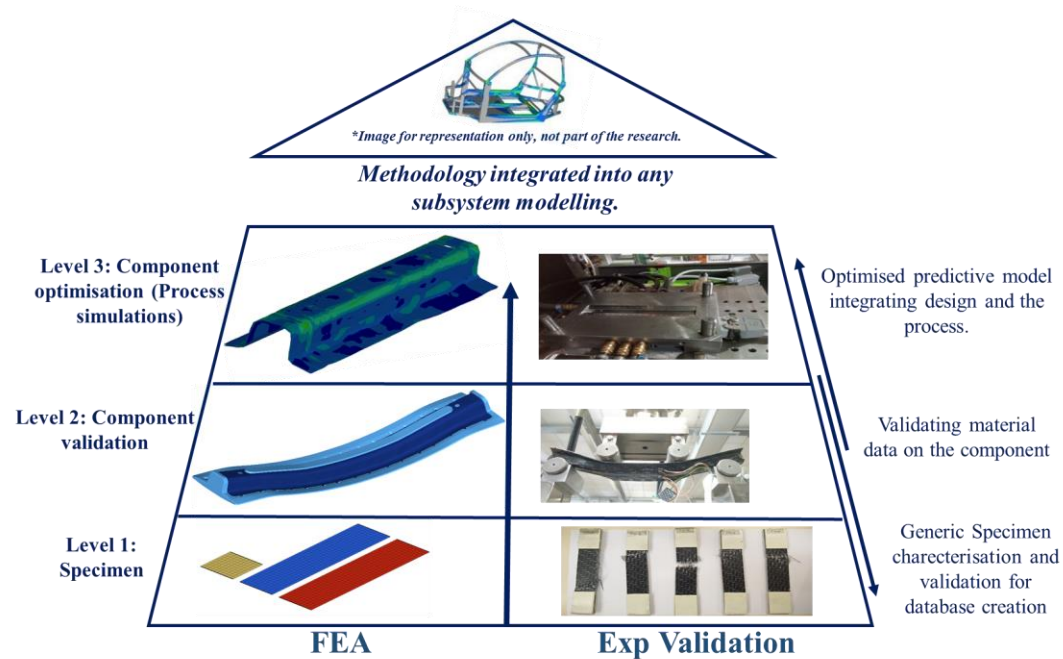
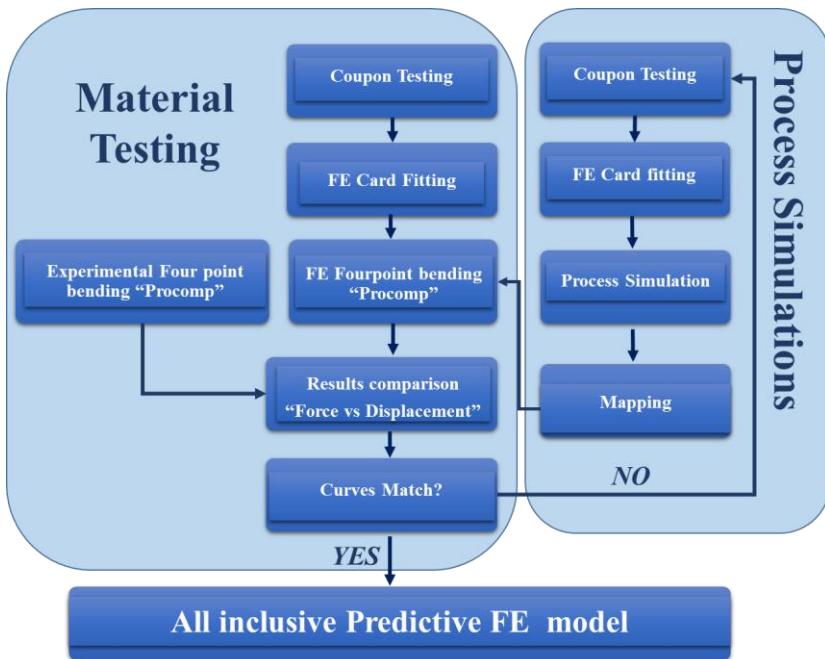


DIMEAS - MECHANICS AND AEROSPACE ENGINEERING DEPARTMENTS
«**I**NNOVATIVE **E**LECTRIC AND **H**YBRID **V**EHICLES»
RESEARCH GROUP

Modelling and testing of Thermoplastic composite parts integrating process simulation

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(S221262)*

Coordinator: Prof. Luigi Garibaldi
Tutor: Prof. Massimiliana Carello



Level 1: Material FEA and Experimental tests

5 Specimens tested for each behaviour



a: Tensile Test
ASTM D 3039



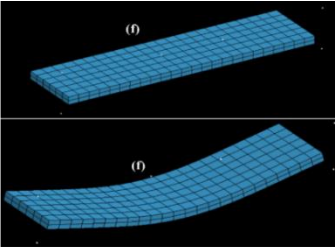
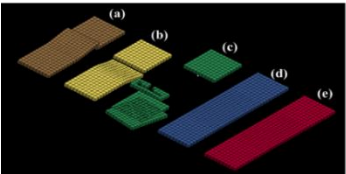
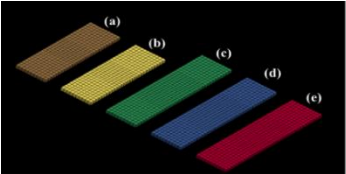
b: Compression Test
ISO14126:1999



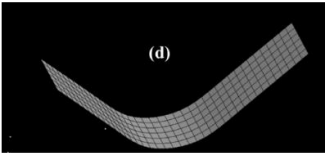
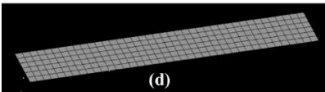
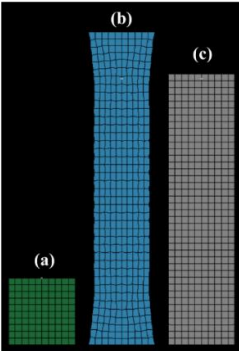
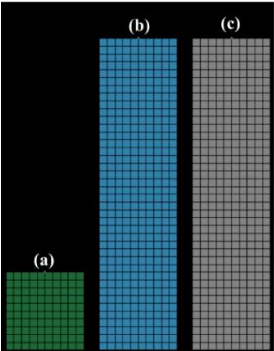
c: Bending Test
ISO 14125:1998



d: Shear Test
ISO 14129: 1997

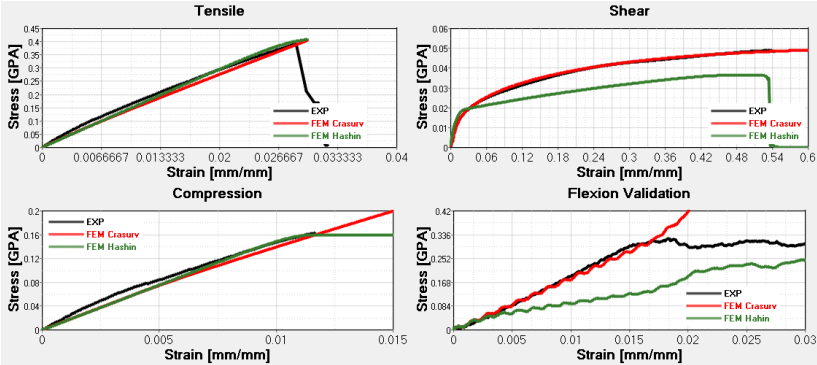


(a) Compression 0° test
(b) Compression 90° test
(c) Shear test
(d) Tensile 0° test
(e) Tensile 90° test
(f) Flexion test validation

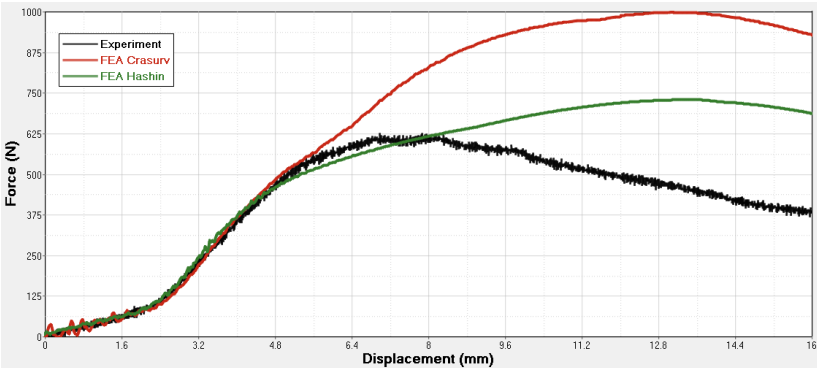


(a) Compression test
(b) Shear test
(c) Tensile test
(d) Flexion test validation

Level 2: Card fitting & component testing



Specimens Material Card



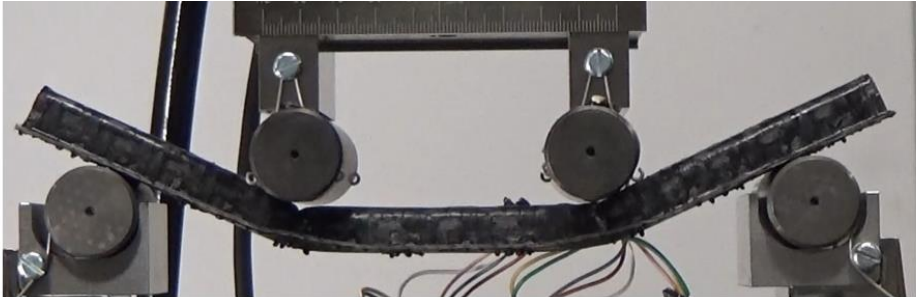
Component Force vs. Displacement Curves

CRASURV (modified Tsai-Wu Formulation)

- Orthotropic plasticity hardening Based on Tsai-Wu
- Quadratic, interactive stress-based criterion
- Failure criteria not directly associated with failure modes.
- Do not take into account different damage mechanisms leading to failure

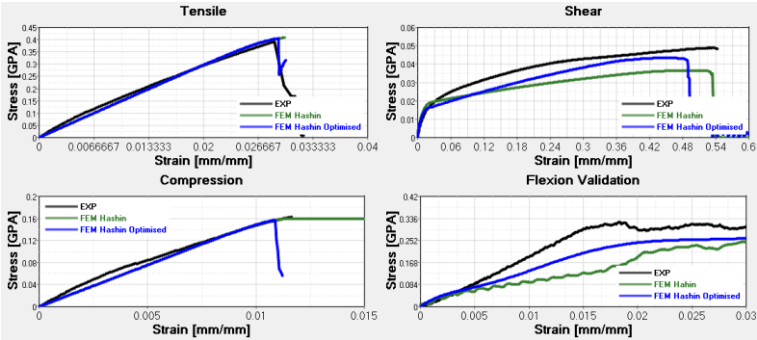
Hashin failure criteria

- Failure criteria associated with failure modes.
- Considers non-homogenous character of composites leading to failure.
- Considers fibre fracture, transverse matrix cracking and shear matrix cracking.

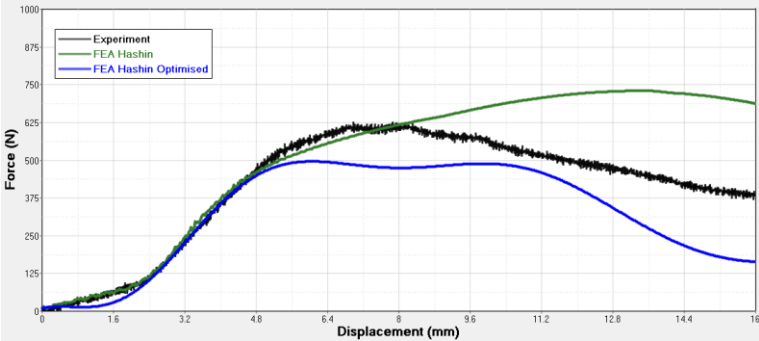


Four-point bending experimental test on component

Level 2: Card fitting optimisation & Component testing



Specimens Material Card

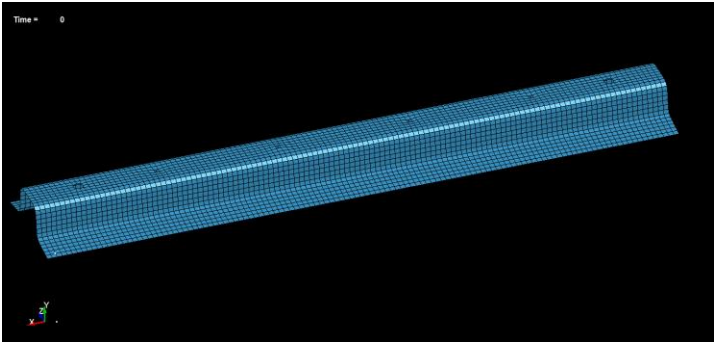


Component Force vs. Displacement Curves

Hashin: Optimised

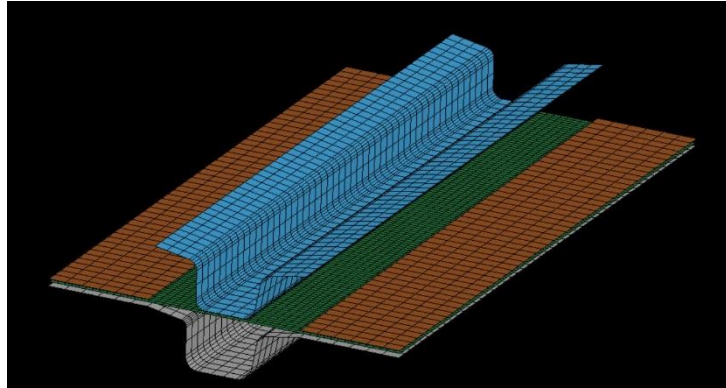
- Optimisation considerations for Hashin for better results match.
- Different failure modes identified and implemented for optimum fit.
- Shear strength increased slightly for a better fit which is validated with the flexion curve.

Overall for a better composite fit a polynomial criterions such as CRASURV (Tsai-Wu) can be safely discarded for Hashin as detailed, where the composite failure can be distinguished individually.



Four-point bending FEA on component

LEVEL 3: Process Simulations and mapping



Process simulation Setup

- Process simulation setup to simulate the thermoforming of composite laminate
- Material model of blank at forming temperature: additive split between isotropic, elasto-plastic matrix and anisotropic hyper-elastic fibers.
- Process parameters required for process simulation:
 - Tensile modulus and the associated tensile curve.
 - Shear modulus and the associated shear curve.
 - Resin parameters at forming temperature.
 - Bending modulus.
 - Frictional coefficients (dynamic and static).



heating



positioning



forming

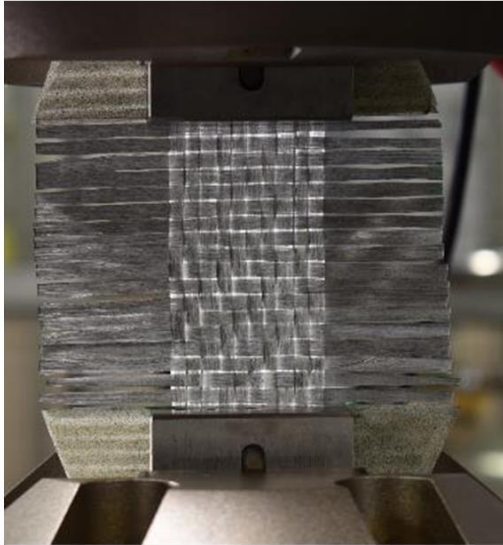
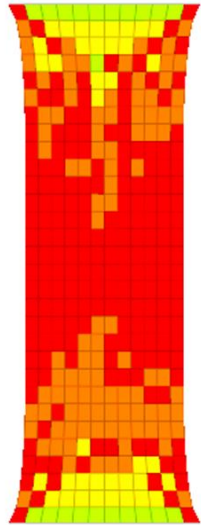


cooling



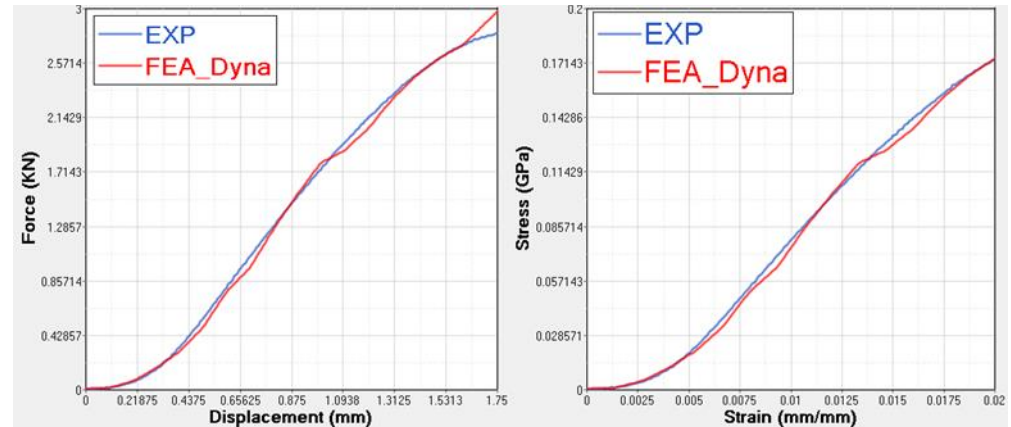
final part

Tensile Tests on Fabric material



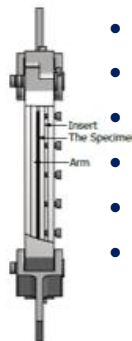
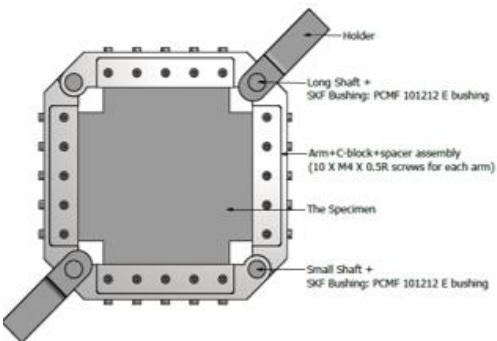
Simulation and Tensile tests (ASTM D5035)

- *5 specimens tested.*
- *Tensile test done for fabric material (not for laminate).*
- *Tensile test results assumed to be the same for both dry fabric and laminate at melting temperature.*

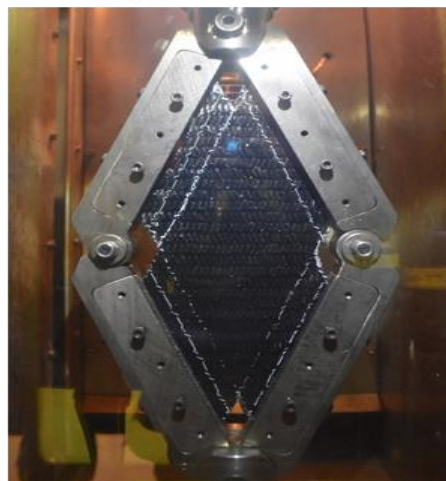
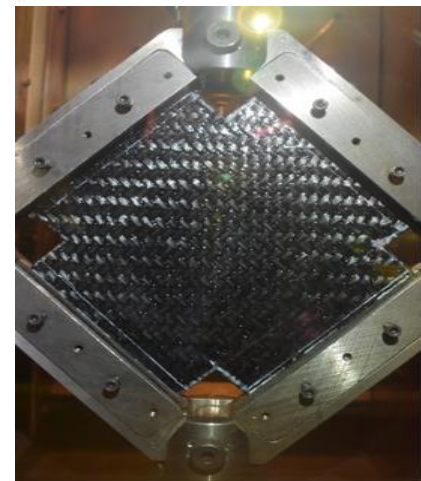


Tensile curve fitting

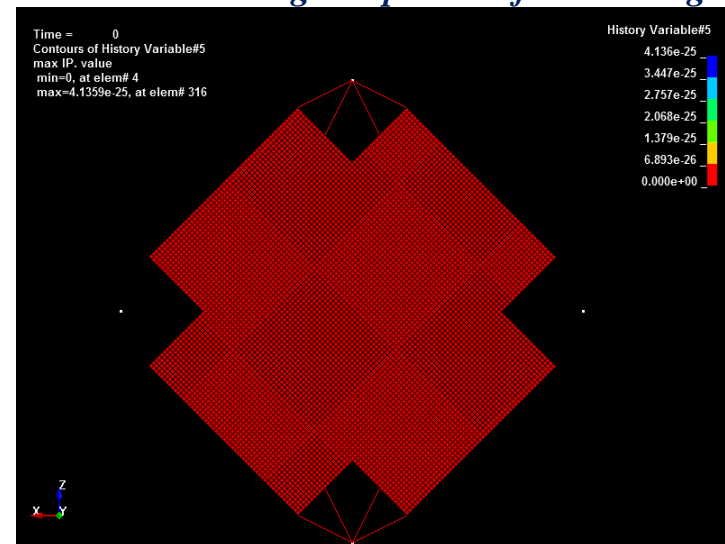
Shear Tests: Trellis Frame



- *Shear induced on a fabric using support on all four sides.*
- *5 specimens tested.*
- *Done on both fabric material and laminate.*
- *Fabric testing: pure shear properties*
- *Laminate: fabric shear properties + resin properties*
- *Difficult level: Complications involved in avoiding compressive forces along the edge on the specimen.*



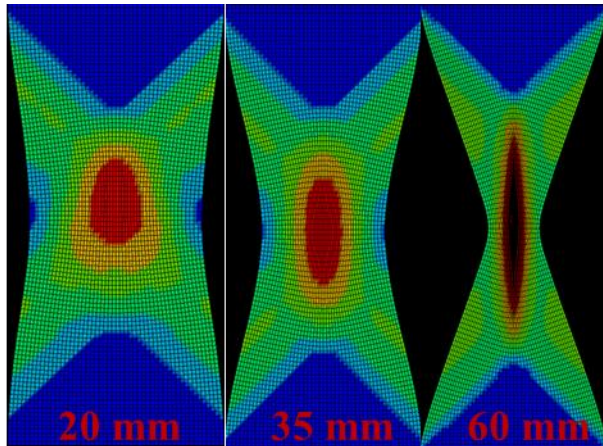
Trellis Frame Laminate in thermal chamber



Trellis Frame FEA

Shear Tests: Bias Extension

- *Modified tensile fixture.*
- *5 specimens tested.*
- *Inducing shear on it at the centre of a specimen oriented at 45°*
- *Tested only for fabric material (not suited for laminate).*
- *Difficult level: Complications involved in material handling, test is material dependant.*



Displacement at various instances: FEA

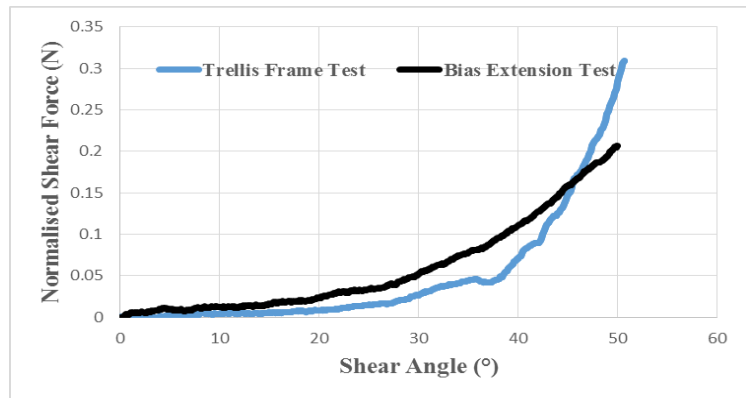


Bias Specimen

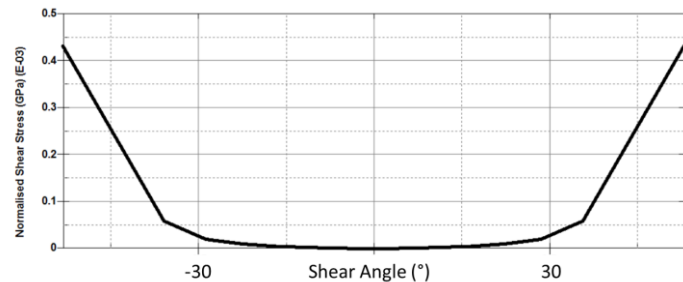


Bias extension test setup

Shear Tests: result validation



Shear force vs. shear angle

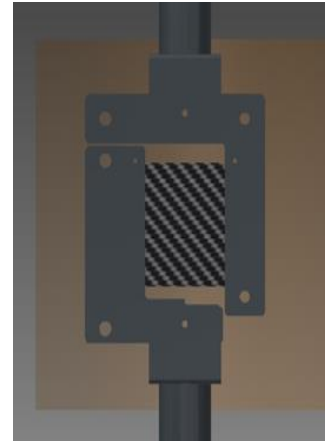


Normalized shear stress vs. shear angle for FE Input

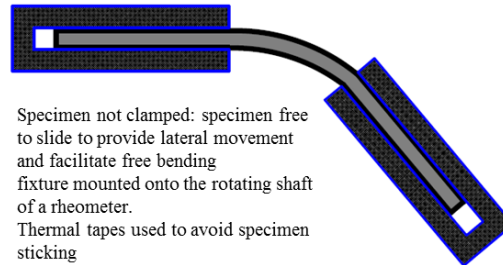
- *Shear properties validated by comparing the shear results from Trellis and Bias extension test.*
- *Shear force normalised.*
- *Shear angle obtained by Digital image correlation and the pattern validated mathematically.*
- *Done as there is no standard for both the tests and this is the best way for validation*

Bending Test: Custom dynamic bending testing fixture

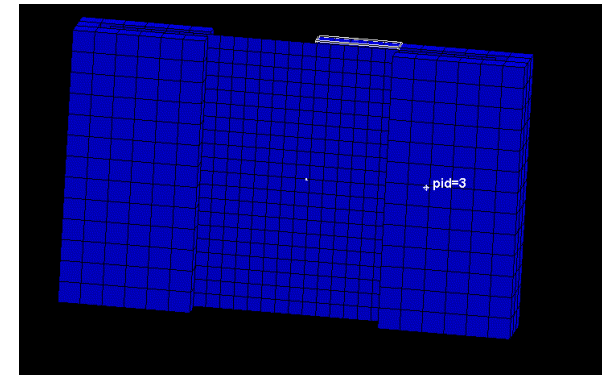
- *Custom made components for bending tests.*
- *5 specimens tested.*
- *Validating the bending behaviour of composite at forming temperature.*
(traditional bending tests impractical at forming temperature).
- *“Integration point position variation method” for determining the ideal bending stiffness.*



Development and testing of the bending fixture



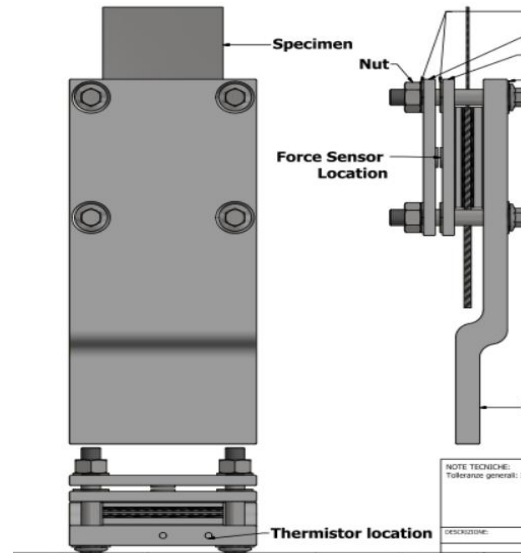
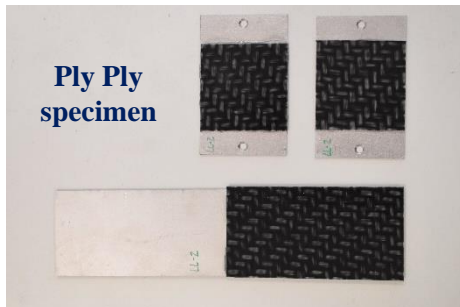
- Specimen not clamped: specimen free to slide to provide lateral movement and facilitate free bending
- fixture mounted onto the rotating shaft of a rheometer.
- Thermal tapes used to avoid specimen sticking



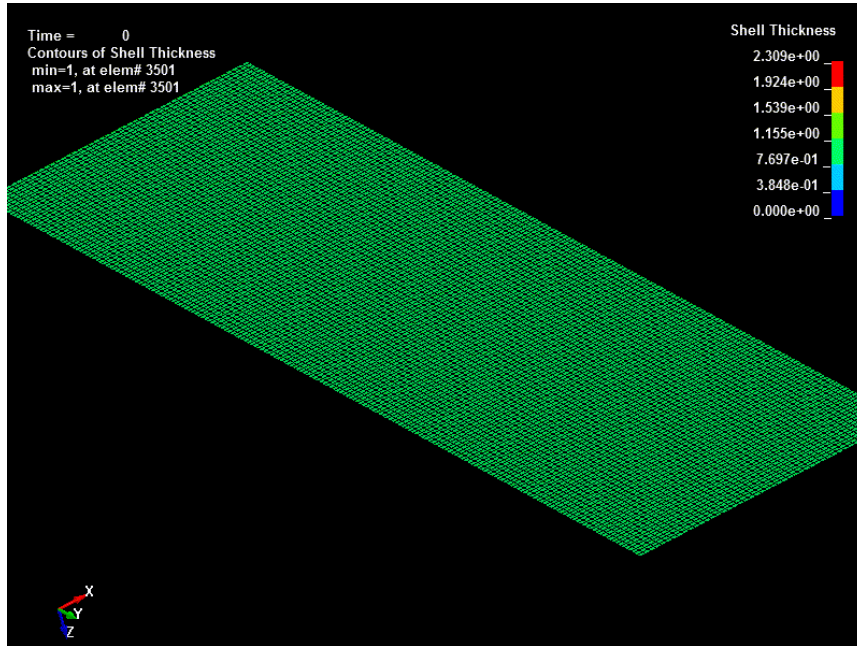
Bending Fixture FEA

Friction tests: Custom Ply-Ply and Tool-Ply Tests

- *Custom made components for friction tests*
- *5 specimens tested.*
- *To obtain frictional coefficients (Static and dynamic) for*
 - *Between tool and ply*
 - *Between ply and ply*
- *Using a high temperature piezoelectric force sensor*
- *Easy to implement in any testing machine inside a thermal chamber for testing.*



LEVEL 3: Thermoforming simulations



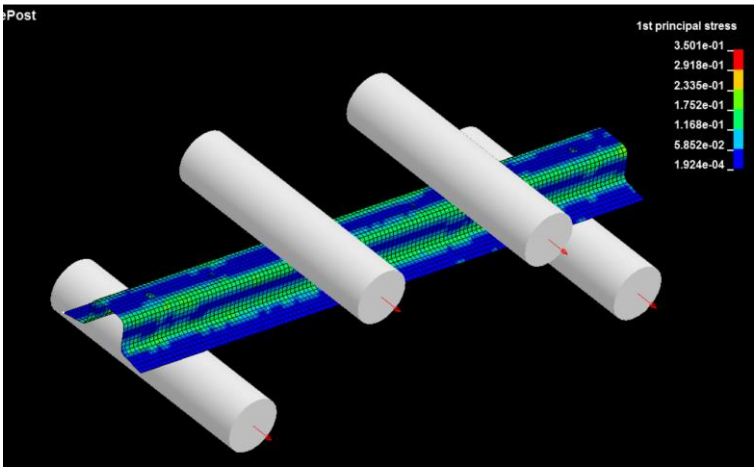
Process simulation conducted to identify:

- *Geometric non-linearities*
 - *Residual stresses and strains*
 - *Fabric orientation change*
 - *Thickness change*
 - *Buckling.*
- *Boundary non-linearities*
 - *Frictional wear from contact between tool and ply*

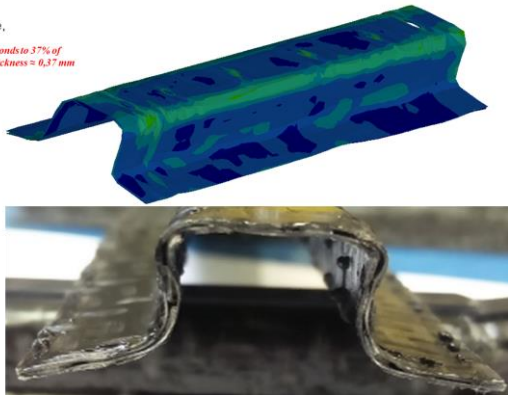
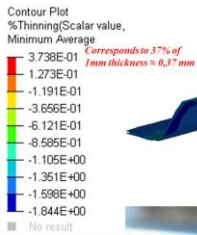
LEVEL 3: Thermoforming results Mapping

Mapping

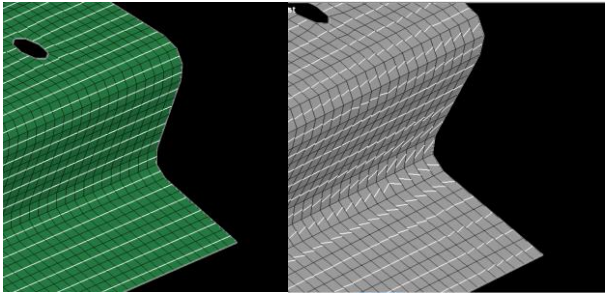
Transfer of the required process simulation data to the crash model for further structural analysis



Mapped residual stresses

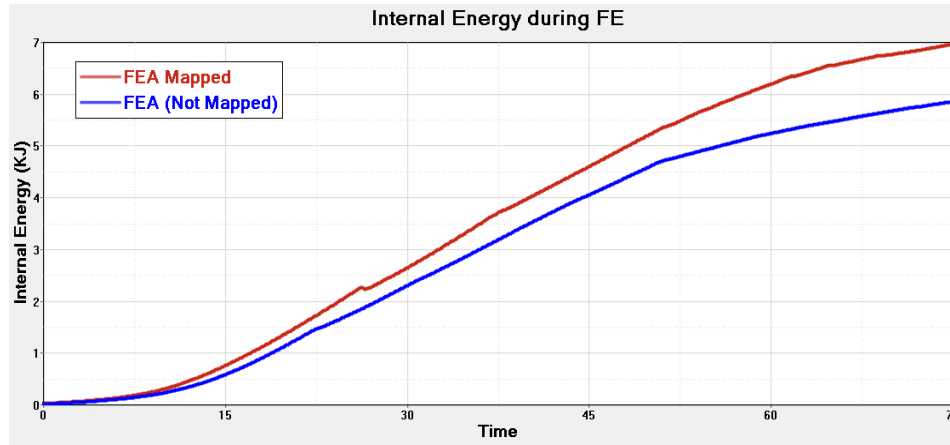


Thickness variation comparison



Element Direction: Before and after Mapping

LEVEL 3: Component four point bending curves comparison after mapping



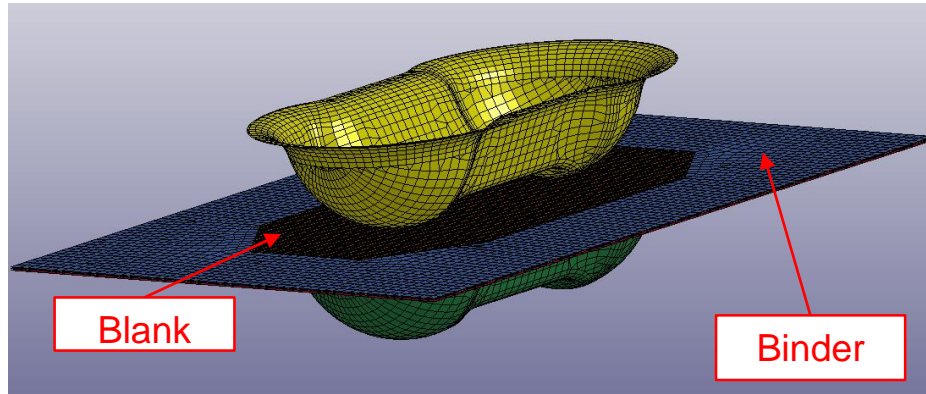
The two main reasons for variation in result after mapping:

- *Fibre orientation change*
- *Presence of residual stresses*
 - *Micro-mechanical level*
 - *Macro-mechanical level*
 - *Global level*

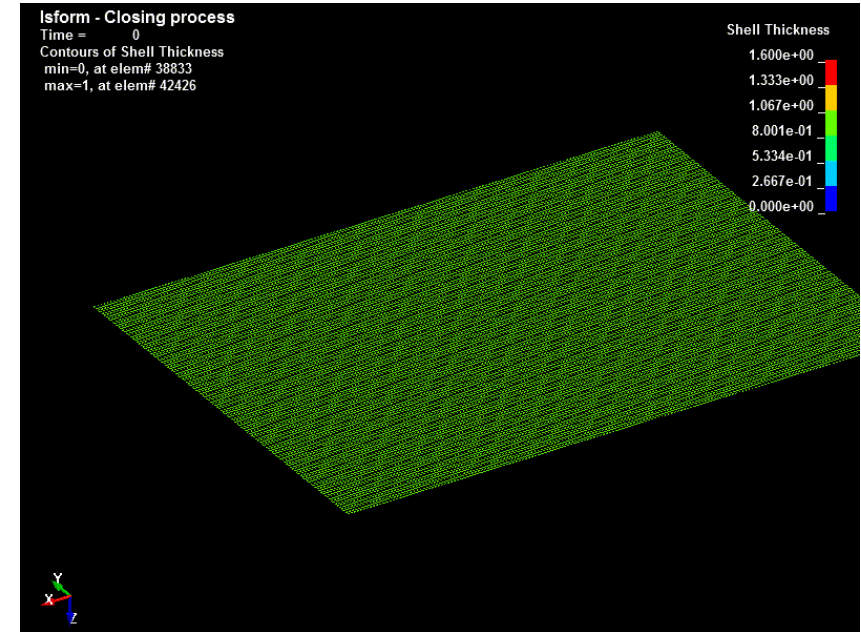
Conclusions

- *The component failure strength increases slightly after mapping*
- *Due to the thickness change and the presence of compressive residual stresses which strenghtens and tolerates the applied force a bit longer*

Thermoforming Methodology Validation: a Doubledome case



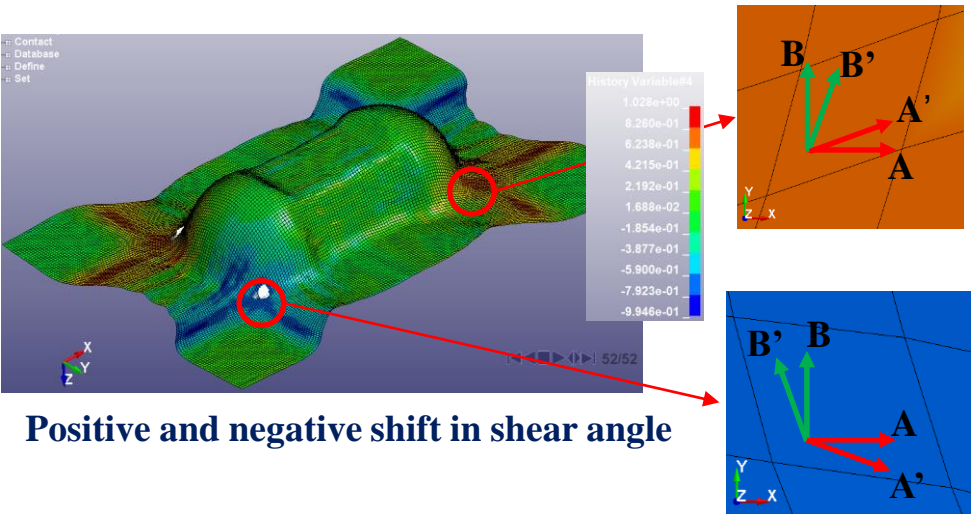
Thermoforming doubledome setup



Thermoforming doubledome simulation

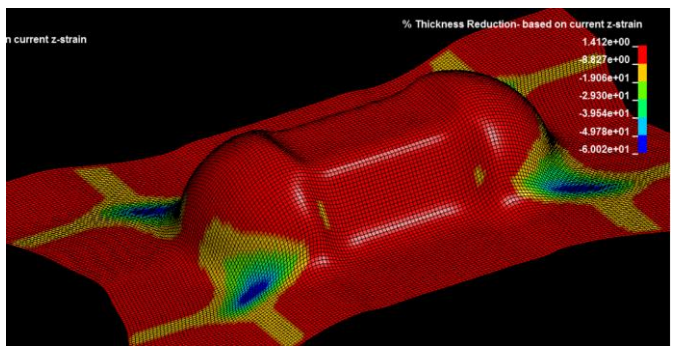
- *Done specifically to validate the methodology*
- *Shows the importance of including the process simulation results in load and crash FEA*

Influence of process simulation Results: a Doubledome case

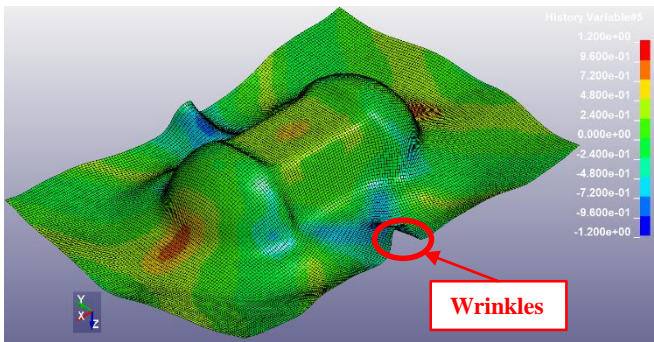


Positive and negative shift in shear angle

- The figures displays the various anomalies occuring on the part, that affects the structural stiffness of the doubledome*
- So it is very important, for an accurate predictive model, include the results from process simulations.*

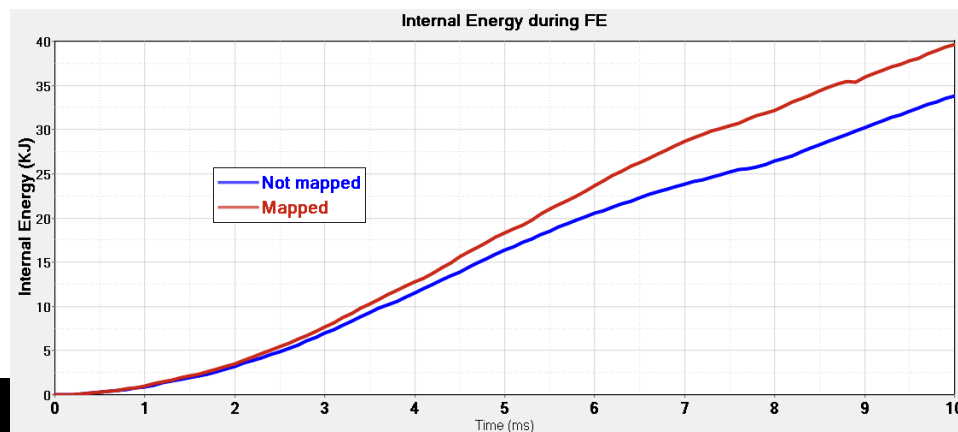


% thickness reduction on the blank after forming



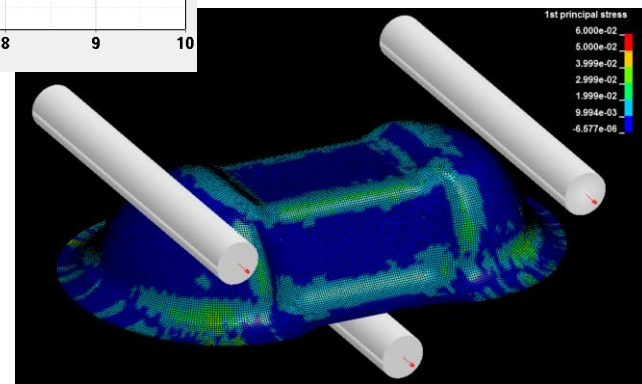
Formation of wrinkles on the blank

Doubledome Structural simulations: results comparison



- The strength of the double dome increases slightly.*
- Due to the thickness change and the presence of compressive residual stresses preventing brittle fracture as the initial crack is formed under compressive (negative tensile) stress.*

Three point bending: no residual stress

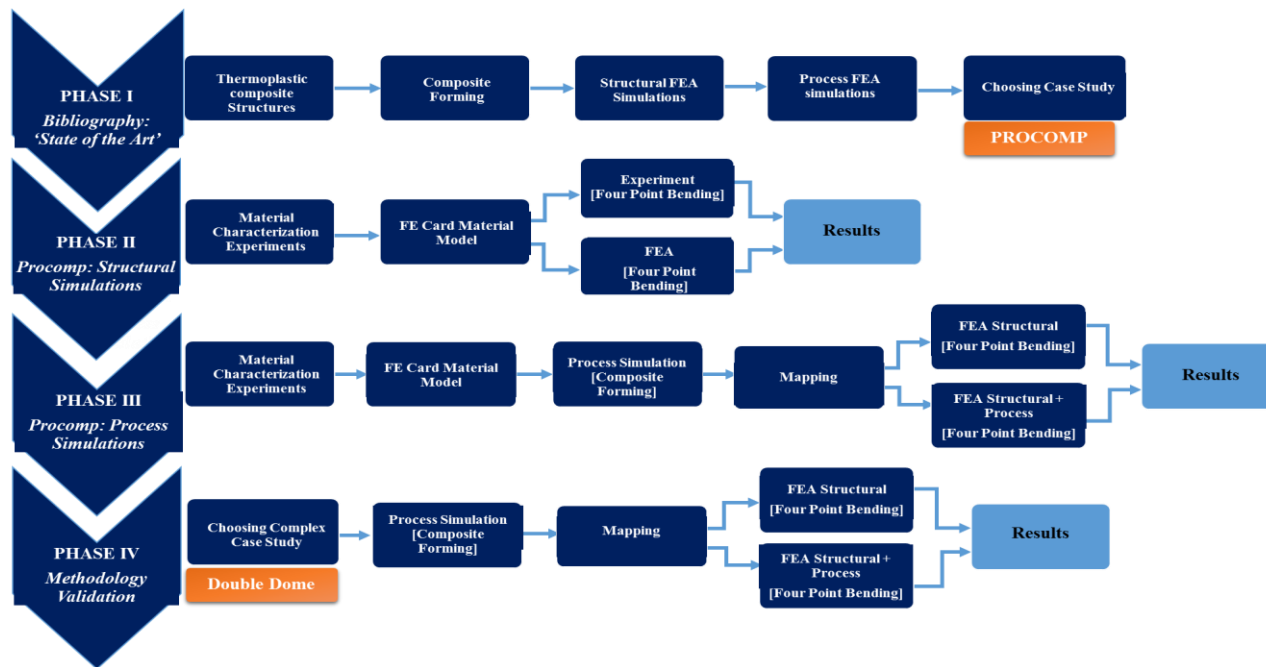


Three point bending: with residual stress
and fabric direction mapped

Research Conclusions

- *Composite failure criteria such as Tsai-wu or Crasurv which is not directly associated with failure modes didnot give good results for out of plane bending of the curved laminate.*
- *Hashin criterion, a failure crtieria directly associated with failure modes gives acceptable results.*
- *Successfull implementation of all the necessary tests for process simulations such as Tensile tests, Trellis frame, Bias test, Bending test and friction test.*
- *Successfull mapping of the process simulation data on to the model gives a fairly accurate result for further four point bending FE tests, giving a good match with experimental curve.*
- *The effect of residual stresses and fibre direction changing validated again with a more complex double dome model.*

Research in brief



Thank You

<i>Lessons attended</i>	<i>Credit</i>
<i>Communication</i>	<i>1</i>
<i>Durability and Ageing of Organic Matrix Composites (OMC)</i>	<i>2</i>
<i>Multiscale structural mechanics</i>	<i>3</i>
<i>Probabilità applicata e processi stocastici</i>	<i>6</i>
<i>Progettazione di strutture meccaniche in materiale composito</i>	<i>6</i>
<i>Programmazione degli esperimenti industriali</i>	<i>5</i>
<i>Public speaking 1 & 2</i>	<i>3</i>
<i>Strumenti e applicazioni del systems engineering</i>	<i>6</i>
<i>Strumenti e tecnologie per lo sviluppo del prodotto</i>	<i>5</i>
<i>The redefinition of the International System of Units (SI)</i>	<i>3</i>
<i>Topics In Internet & Society Interdisciplinary Studies</i>	<i>4</i>
<i>Polymers and Polymer Matrix Composites in Harsh Environments</i>	<i>2</i>
<i>Lingua Italiana I Livello</i>	<i>3</i>
<i>Total Credits (Exceeded)</i>	<i>49</i>

RESEARCH AND CONFERENCE PAPERS

- Carello, M., Amirth, N., Airale, A.G. et al. Appl Compos Mater (2017). Building Block Approach ' for Structural Analysis of Thermoplastic Composite Components for Automotive Applications doi:10.1007/s10443-017-9592-x
- Carello, M.; Airale, A.G.; Ferraris, A.; Messina, A.; Amirth Jayasree, N. (2017) From thermosetting to thermoplastic composite materials: automotive applications in structural components. In: Automotive Engineering Congress, Norimberga (Germany), 30-31 March 2017.
- N. Amirth Jayasree, A.G. Airale, A. Ferraris, A. Messina, L. Sisca, M. Carello. (2017). Process analysis for structural optimisation of thermoplastic composite component using the building block approach. Composites Part B: Engineering. 126, 119-132.